

# On Stability Criteria of Explicit Difference Schemes for Certain Heat Conduction Problems with Uncommon Boundary Conditions

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**Abstract.** Stability criteria are derived for the explicit difference schemes appropriate to the following problems: 1) heat conduction in a slab in contact with a well stirred liquid; 2) heat conduction in a slab radiating to one face of a thin slab with infinite thermal conductivity, the other face of which radiates into a medium at prescribed temperature; 3) heat conduction in a cylinder radiating to the inner surface of a thin coaxial cylindrical shell with infinite thermal conductivity, the outer surface of which radiates into a medium at prescribed temperature.

Although the exact analytical solutions of certain problems in heat conduction involving complicated boundary conditions are known, the complexity of the analytical expressions is often such as to make them impractical for the numerical evaluation of the solutions. This is for instance the case of the writer's solution of the problem of "heat conduction in a solid in contact with a well stirred liquid" [1]. It is also the case of the problems treated by Walter P. Reid and dealing with the heat conduction in a semi-infinite solid (or cylinder) when the boundary surface radiates to one boundary surface of a thin slab (or thin cylindrical shell), with infinite thermal conductivity, the other boundary surface of which radiates into a medium at prescribed temperature [2], [3].

To obtain numerical answers to the above problems it is expedient to evaluate the solutions of the appropriate explicit difference analogs. The object of this report is to derive the stability criteria for the difference schemes appropriate to the problems above-mentioned.

Consider first the problem of heat conduction in a slab one face of which is in contact with a well-stirred liquid. For the sake of concreteness we shall first assume that the other face is kept at  $0^{\circ}\text{C}$ . The mathematical formulation of the problem is as follows:

$$(1) \quad \frac{\partial T}{\partial t} = k \frac{\partial^2 T}{\partial x^2} \quad 0 \leq x \leq a, \quad t > 0$$

$$(2) \quad T(x, 0) = f(x)$$

$$(3A) \quad T(0, t) = 0$$

$$(4) \quad -\frac{\partial T}{\partial x} = \left( \frac{\rho_0 c_0 d}{K} \right) \frac{\partial T}{\partial t} = \sigma \frac{\partial T}{\partial t} \quad (\text{say}) \text{ for } x = a.$$

In (4) we have the boundary condition appropriate to the case where the face  $x = a$  is in contact with a layer of a well-stirred liquid of width  $d$ , density  $\rho_0$  and specific heat  $c_0$ . The constants  $K$  and  $k$  are the thermal conductivity and thermal diffusivity of the slab, respectively.

Received August 17, 1959; revised November 4, 1960.



(8) when during some time step an inaccurate vector  $T_k^*$  (where  $k$  can of course be  $= 0$ ) is used in lieu of the true  $T_k$ . It may be briefly mentioned that the above stability criterion is equally valid in case of boundary conditions of the form

$$(3C) \quad \frac{\partial T}{\partial x} = 0 \quad \text{for } x = 0$$

$$(3D) \quad \frac{\partial T}{\partial x} = hT \quad \text{for } x = 0.$$

In the case of the boundary condition (3C) the first element of the first row of the matrix  $A$  is replaced by  $1 - r$ ; in the case of the boundary condition (3D) the element in question is replaced by  $1 - 2r + \alpha r$  where  $\alpha = 1/(1 + h\Delta x)$ . In either case the largest of the sums of the absolute values of the elements of the rows of  $A$  is still equal to one and therefore the stability condition is satisfied if  $r \leq \frac{1}{2}$ . For a discussion of convergence the reader is referred to [4], Section VI.

Consider now the problem of heat conduction in a slab subject to the conditions stipulated in the first of Reid's articles mentioned above. The mathematical formulation of the problem is as follows:

$$(10) \quad \frac{\partial T}{\partial t} = k \frac{\partial^2 T}{\partial x^2} \quad 0 \leq x \leq a, t > 0$$

$$(11) \quad T(x, 0) = f(x)$$

$$(12) \quad T(0, t) = 0$$

$$(13) \quad -K \left( \frac{\partial T}{\partial x} \right)_{x=a} = h_1 [T(a, t) - v(t)]$$

$$(14) \quad \rho_0 c_0 d \frac{\partial v}{\partial t} = h_1 [T(a, t) - v(t)] - h_2 v(t)$$

$$(15) \quad v(0) = V$$

In the above:

$K$  = thermal conductivity of the thick slab

$k$  = thermal diffusivity of the thick slab

$h_1$  = coefficient of heat transfer between the two slabs

$h_2$  = coefficient of heat transfer between the thin slab and the surrounding medium (with temperature zero)

$v(t)$  = temperature of thin slab

$\rho_0, c_0$  and  $d$  are the density, specific heat and width of the thin slab.

If we put

$$(16) \quad \frac{h_1}{K} = b; \quad \frac{h_2}{K} = c; \quad \frac{\rho_0 c_0 d}{K} = \sigma$$

equations (13) and (14) assume the form

$$(13^*) \quad - \left( \frac{\partial T}{\partial x} \right)_{x=a} = b [T(a, t) - v(t)]$$

$$(14^*) \quad \sigma \frac{\partial v}{\partial t} = b [T(a, t) - v(t)] - cv(t).$$

We shall investigate the stability of the explicit difference scheme

$$\frac{T_{m,n+1} - T_{m,n}}{\Delta t} = \frac{k}{(\Delta x)^2} (T_{m-1,n} - 2T_{m,n} + T_{m+1,n})$$

or

$$(17) \quad T_{m,n+1} = rT_{m-1,n} + (1 - 2r)T_{m,n} + rT_{m+1,n}, \quad m = 1, 2, 3, \dots, M$$

where

$$T_{m,n} = T(m\Delta x, n\Delta t), \quad r = \frac{k\Delta t}{(\Delta x)^2} \quad \text{and} \quad \Delta x = \frac{a}{M+1}.$$

The difference analogs of (13\*) and (14\*) are

$$\frac{T_{M,n} - T_{M+1,n}}{\Delta x} = b(T_{M+1,n} - v_n)$$

or

$$(18) \quad T_{M+1,n} = \frac{1}{1 + b\Delta x} T_{M,n} + \frac{b\Delta x}{1 + b\Delta x} v_n = pT_{M,n} + qv_n \quad (\text{say})$$

and

$$\sigma \frac{v_{n+1} - v_n}{\Delta t} = bT_{M+1,n} - (b + c)v_n$$

or

$$(19) \quad v_{n+1} = \frac{b\Delta t}{\sigma} T_{M+1,n} + \left[ 1 - \frac{(b + c)\Delta t}{\sigma} \right] v_n = \alpha T_{M+1,n} + \beta v_n \quad (\text{say})$$

where we have written  $v_n$  and  $v_{n+1}$  for  $v(n\Delta t)$  and  $v[(n + 1)\Delta t]$ , respectively. If from (18) and (19) we eliminate  $T_{M+1,n}$  we get

$$(20) \quad v_{n+1} = \alpha p T_{M,n} + (\beta + \alpha q)v_n.$$

If we rewrite (18) in the form

$$(18^*) \quad T_{M+1,n+1} = pT_{M,n+1} + qv_{n+1}$$

and eliminate  $v_n$  and  $v_{n+1}$  from (18\*), (18), and (19), we get

$$(21) \quad T_{M+1,n+1} = (\beta + \alpha q)T_{M+1,n} + pT_{M,n+1} - p\beta T_{M,n}.$$

If in (21) we replace  $T_{M,n+1}$  by its expression from (17) with  $h = M$ , we ultimately get

$$(22) \quad \begin{aligned} T_{M+1,n+1} &= prT_{M-1,n} + p(1 - 2r - \beta)T_{M,n} + (pr + \beta + \alpha q)T_{M+1,n} \\ &= PT_{M-1,n} + QT_{M,n} + ST_{M+1,n} \quad (\text{say}). \end{aligned}$$

Starting with the values of  $T_{m,n}$  for  $n = 0$  equations (17) and (22) will generate in succession the values of  $T_{m,n}$  for  $n = 1, 2, \dots$  and  $m = 1, 2, 3, \dots, M + 1$ . Similarly, starting with  $v(t) = V$  for  $t = 0$  equation (19) will generate in succession the values of  $v_n = v(n\Delta t)$ .



Finally, consider the problem of heat conduction in a cylinder subject to the boundary conditions stipulated in the second of Reid's articles mentioned above.

If, for the sake of convenience, we denote by  $x$  the radial distance ordinarily denoted by  $r$ , the mathematical formulation of the problem is as follows:

$$(30) \quad \frac{\partial T}{\partial t} = k \left( \frac{\partial^2 T}{\partial x^2} + \frac{1}{x} \frac{\partial T}{\partial x} \right)$$

$$(31) \quad T(x, 0) = f(x)$$

$$(32) \quad \frac{\partial T}{\partial x} = 0 \quad \text{for } x = 0$$

$$(33) \quad -K \left( \frac{\partial T}{\partial x} \right)_{x=a} = m_1 [T(a, t) - v(t)]$$

$$(34) \quad 2\pi\rho_0 c_0 a \frac{dv}{dt} = m_1 [T(a, t) - v(t)] - m_2 v(t).$$

The only essential difference between the above problem for the cylinder and the corresponding problem for the slab is the differential equation (30) which takes the place of (10) and the new condition (32). The difference analogs of (30) and (32) are

$$\frac{T_{m,n+1} - T_{m,n}}{\Delta t} = k \left[ \frac{T_{m-1,n} - 2T_{m,n} + T_{m,n+1}}{(\Delta x)^2} + \frac{1}{m\Delta x} \cdot \frac{T_{m+1,n} - T_{m-1,n}}{2\Delta x} \right]$$

or

$$(35) \quad T_{m,n+1} = r \left( 1 - \frac{1}{2m} \right) T_{m-1,n} + (1 - 2r) T_{m,n} + r \left( 1 + \frac{1}{2m} \right) T_{m+1,n}$$

$m = 1, 2, 3, \dots M$

and

$$(36) \quad T_{0,n} = T_{1,n}.$$

The difference equation (35) takes the place of the difference equation (17). In view of (35) and (36) it is readily seen that the previous developments for the slab may be carried out with the sole exception that in lieu of (24) the matrix  $A$  is now

$$(37) \quad A = \begin{bmatrix} 1 - 2r & \frac{3}{2}r & & & \\ \left(1 - \frac{1}{4}\right)r & 1 - 2r & \left(1 + \frac{1}{4}\right)r & & \\ & \left(1 - \frac{1}{6}\right)r & 1 - 2r & \left(1 + \frac{1}{6}\right)r & \\ & \dots\dots\dots & \dots\dots\dots & \dots\dots\dots & \\ & & \left(1 - \frac{1}{2M}\right)r & 1 - 2r & \left(1 + \frac{1}{2M}\right)r \\ & & P & Q & S \end{bmatrix}$$

where the symbols  $P$ ,  $Q$ , and  $S$  have the same significance as before. Since for the first  $M$  rows of  $A$  the largest of the sums of the absolute values of the elements is

equal to 1 (provided  $r \leq \frac{1}{2}$ ) we reach the conclusion that the criteria of stability are identical with those of the previous problem and are given in the inequalities (28) and (29).

It may be briefly mentioned that the above analysis of stability may be readily extended to the case where the cylinder and the coaxial thin cylindrical shell are replaced by a sphere and a concentric thin spherical shell.

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